

ENVELOPE EQUATIONS

◆ **Transverse envelope equations**

- 1-dimensional (8 Slides)
- 2-dimensional => Coupled oscillations of the transverse beam sizes (8)

◆ **Longitudinal envelope equation**

- Longitudinal envelope equation far from transition (4)
- Evolution of the phase space ellipse near transition, without collective effects (16)
- Longitudinal envelope equation near transition (6)
- Bunch rotation with (or without) SC (and or BB impedance) (7)

TRANSVERSE ENVELOPE EQUATIONS (1/16)

- ◆ Consider a particle in an ensemble of particles which obeys the single-particle equations

$$x' = p_x$$

$$p_x' = \frac{F_x(x, s)}{\beta^2 E_{total}}$$

- ◆ The total force is $F_x(x, s) = F_x^{ext} + F_x^{SC}$

- ◆ Let's consider a particle distribution $f(x, p_x, s)$. Averaging over the particle distribution, we obtain the equations of motion for the centre of the beam

$$\langle x \rangle' = \langle p_x \rangle$$

$$\langle p_x \rangle' = \frac{\langle F_x(x, s) \rangle}{\beta^2 E_{total}} = \frac{\langle F_x^{ext} \rangle}{\beta^2 E_{total}}$$

as $\langle F_x^{SC} \rangle = 0$, because of Newton's 3rd law

TRANSVERSE ENVELOPE EQUATIONS (2/16)

- ◆ For a linear machine, one has

$$\frac{F_x^{ext}}{\beta^2 E_{total}} = -K_x(s) x$$

$$\rightarrow \langle x \rangle'' + K_x(s) \langle x \rangle = 0$$

- ◆ The 2nd moments satisfy the equations

$$\langle x^2 \rangle' = 2 \langle x x' \rangle = 2 \langle x p_x \rangle$$

$$\langle x p_x \rangle' = \langle x' p_x \rangle + \langle x p_x' \rangle = \langle p_x^2 \rangle - K_x(s) \langle x^2 \rangle + \langle x \frac{F_x^{SC}}{\beta^2 E_{total}} \rangle$$

$$\langle p_x^2 \rangle' = 2 \langle p_x p_x' \rangle = -2 K_x(s) \langle x p_x \rangle + 2 \langle p_x \frac{F_x^{SC}}{\beta^2 E_{total}} \rangle$$

TRANSVERSE ENVELOPE EQUATIONS (3/16)

- To study space-charge effects, we are interested in the position and momentum offsets of the particle from their respective averages, i.e.

$$\Delta x = x - \langle x \rangle$$

$$\Delta p_x = p_x - \langle p_x \rangle$$



$$\langle \Delta x^2 \rangle' = 2 \langle \Delta x \Delta p_x \rangle$$

$$\langle \Delta x \Delta p_x \rangle' = \langle \Delta p_x^2 \rangle - K_x(s) \langle \Delta x^2 \rangle + \langle \Delta x \frac{F_x^{SC}}{\beta^2 E_{total}} \rangle$$

$$\langle \Delta p_x^2 \rangle' = -2 K_x(s) \langle \Delta x \Delta p_x \rangle + 2 \langle \Delta p_x \frac{F_x^{SC}}{\beta^2 E_{total}} \rangle$$

- Define the rms beam emittance

$$\varepsilon_{x,rms} = \sqrt{\langle \Delta x^2 \rangle \langle \Delta p_x^2 \rangle - \langle \Delta x \Delta p_x \rangle^2}$$

and rms beam size

$$\sigma_x = \sqrt{\langle \Delta x^2 \rangle}$$

TRANSVERSE ENVELOPE EQUATIONS (4/16)



$$\langle \Delta p_x^2 \rangle = \frac{\varepsilon_{x,rms}^2 + \langle \Delta x \Delta p_x \rangle^2}{\langle \Delta x^2 \rangle}$$

$$\sigma'_x = \frac{\langle \Delta x \Delta p_x \rangle}{\sqrt{\langle \Delta x^2 \rangle}}$$

$$\sigma''_x = \frac{\langle \Delta x \Delta p_x \rangle'}{\sqrt{\langle \Delta x^2 \rangle}} - \frac{\langle \Delta x \Delta p_x \rangle^2}{\langle \Delta x^2 \rangle^{3/2}}$$

- ◆ Finally, the transverse envelope equation can be obtained

$$\sigma''_x + K_x(s) \sigma_x - \frac{\varepsilon_{x,rms}^2}{\sigma_x^3} - \frac{\langle \Delta x F_x^{SC} \rangle}{\sigma_x \beta^2 E_{total}} = 0$$

TRANSVERSE ENVELOPE EQUATIONS (5/16)

- ◆ The SC force was derived in the previous “SC course” (assuming for instance a uniform transverse distribution and a round beam)

$$\frac{F_x^{SC}}{\beta^2 E_{total}} = \frac{e \lambda}{\beta^2 E_{total} 2 \pi \epsilon_0 \gamma^2} \frac{\Delta x}{a^2}$$

$$a = 2 \sigma_x$$

$$\lambda = \frac{N_b e}{l} = N_l e$$

⇒

$$\frac{F_x^{SC}}{\beta^2 E_{total}} = K_{sc,x2} \frac{\Delta x}{a^2}$$

with

$$K_{sc,x2} = \frac{2 N_l r_p}{\beta^2 \gamma^3}$$

Therefore,

$$\frac{\langle \Delta x F_x^{SC} \rangle}{\beta^2 E_{total}} = \frac{K_{sc,x2}}{4}$$

TRANSVERSE ENVELOPE EQUATIONS (6/16)

- ◆ The 1-dimensional envelope equation can finally be written

$$a'' + K_x(s) a - \frac{\varepsilon_x^2}{a^3} - \frac{K_{sc,x2}}{a} = 0$$

$$a = 2\sigma_x$$

$$\varepsilon_x = 4\varepsilon_{x,rms}$$

- ◆ Effect of space charge on the equilibrium beam size a_0 , in the smooth approximation

$$K_x = (Q_{x0} / R)^2$$

TRANSVERSE ENVELOPE EQUATIONS (7/16)

→ The equilibrium beam size is therefore found from

$$\left(\frac{Q_{x0}}{R} \right)^2 a_0 - \frac{K_{sc,x2}}{a_0} - \frac{\epsilon_x^2}{a_0^3} = 0$$

which yields

$$a_0^2 = \frac{\epsilon_x R}{Q_{x0}} \left(\kappa + \sqrt{1 + \kappa^2} \right)$$

$$\kappa = \frac{K_{sc,x2} R}{2\epsilon_x Q_{x0}}$$

- ◆ The beam size is significantly perturbed by the space-charge force when $\kappa \geq 1$
- ◆ If the beam size becomes larger than the vacuum chamber aperture, there will be a beam loss

TRANSVERSE ENVELOPE EQUATIONS (8/16)

- ◆ For weak beam intensities, i.e. $\kappa \ll 1$

$$a_0^2 = a_{00}^2 + \Delta a_{00}^2$$

with $a_{00}^2 = \frac{\varepsilon_x R}{Q_{x0}}$ $\Delta a_{00}^2 = \kappa a_{00}^2$

- ◆ The parameter a_{00} describes the beam size in the absence of space charge. Interpreting Δa_{00} as a perturbation on the single-particle tune according to $a_0^2 = \varepsilon_x R / (Q_{x0} + \Delta Q_x)$, gives an expression for the shift of the single-particle tune due to space charge

$$\Delta Q_x = - \frac{K_{sc,x2} R}{2 \varepsilon_x}$$

→ It is 1/2 of the result found in the “SC course” with $a = \sqrt{2} \sigma_x$ (as expected)

TRANSVERSE ENVELOPE EQUATIONS (9/16)

- ◆ Let's come back to the general case, i.e. consider a beam with unequal transverse beam sizes => The envelope equations are therefore given by (we saw in the "SC course", that in the SC force, a^2 must be replaced by $a(a+b)/2$)

$$a'' + K_x a - \frac{2K_{sc,x2}}{a+b} - \frac{\epsilon_x^2}{a^3} = 0$$

$$b'' + K_y b - \frac{2K_{sc,x2}}{a+b} - \frac{\epsilon_y^2}{b^3} = 0$$

$$a = 2\sigma_x$$

$$\epsilon_x = 4\epsilon_{x,rms}$$

$$b = 2\sigma_y$$

$$\epsilon_y = 4\epsilon_{y,rms}$$

TRANSVERSE ENVELOPE EQUATIONS (10/16)

→ Both transverse planes have thus to be treated jointly for high-intensity beams due to space-charge coupling

- ◆ The beam may execute some collective motion on top of equilibrium beam sizes a_0 and b_0

$$a(s) = a_0 + \Delta a(s)$$

- ◆ Let the horizontal and vertical beam sizes be

$$b(s) = b_0 + \Delta b(s)$$

where the perturbations Δa and Δb are considered small with respect to the equilibrium sizes

- ◆ Linearizing yields

$$\Delta a'' + K_a \Delta a = K \Delta b$$

$$\Delta b'' + K_b \Delta b = K \Delta a$$

$$K = \frac{2K_{sc,x2}}{(a_0 + b_0)^2}$$

$$K_a = 4K_x - \frac{2K_{sc,x2}(2a_0 + 3b_0)}{a_0(a_0 + b_0)^2}$$

$$K_b = 4K_y - \frac{2K_{sc,x2}(2b_0 + 3a_0)}{b_0(a_0 + b_0)^2}$$

→ The transverse beam sizes execute coupled oscillations

TRANSVERSE ENVELOPE EQUATIONS (11/16)

- ◆ The equilibrium beam sizes a_0 and b_0 are found from the following equations

$$K_x a_0 - \frac{2K_{sc,x2}}{a_0 + b_0} - \frac{\epsilon_x^2}{a_0^3} = 0$$

$$K_y b_0 - \frac{2K_{sc,x2}}{a_0 + b_0} - \frac{\epsilon_y^2}{b_0^3} = 0$$

- ◆ Using the smooth approximation

$$K_x = (Q_{x0} / R)^2$$

$$K_a = (Q_a / R)^2$$

$$K_y = (Q_{y0} / R)^2$$

$$K_b = (Q_b / R)^2$$

and assuming small tune shifts, yields

TRANSVERSE ENVELOPE EQUATIONS (12/16)

$$Q_a = 2Q_{x0} + \Delta Q_a = 2Q_{x0} - \frac{K_{sc,x2} R^2 (2a_0 + 3b_0)}{2Q_{x0} a_0 (a_0 + b_0)^2}$$

$$Q_b = 2Q_{y0} + \Delta Q_b = 2Q_{y0} - \frac{K_{sc,x2} R^2 (2b_0 + 3a_0)}{2Q_{y0} b_0 (a_0 + b_0)^2}$$

- ◆ The coupled equations can be re-written

$$\frac{d^2 \Delta a}{d\phi^2} + Q_a^2 \Delta a = K R^2 \Delta b$$

$$\phi = \Omega_0 t$$

$$\frac{d^2 \Delta b}{d\phi^2} + Q_b^2 \Delta b = K R^2 \Delta a$$

TRANSVERSE ENVELOPE EQUATIONS (13/16)

- ◆ Far from the coupling resonance $Q_a = Q_b$, the solutions of the homogeneous equations (of the coupled oscillations) are given by

$$\Delta a = \Delta a_0 e^{jQ_a \phi}$$

$$\Delta b = \Delta b_0 e^{jQ_b \phi}$$

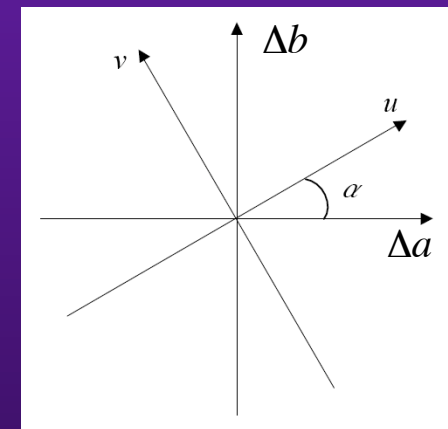
- ◆ In the presence of coupling, the coupled oscillations can be solved by searching the normal (i.e. decoupled) modes (u,v) linked by a simple rotation

$$\begin{pmatrix} \Delta a \\ \Delta b \end{pmatrix} = \begin{bmatrix} \cos \alpha & -\sin \alpha \\ \sin \alpha & \cos \alpha \end{bmatrix} \begin{pmatrix} u \\ v \end{pmatrix}$$

- ◆ The equations of the 2 normal modes can be found

$$\frac{d^2 u}{d\phi^2} + Q_u^2 u = 0$$

$$\frac{d^2 v}{d\phi^2} + Q_v^2 v = 0$$



TRANSVERSE ENVELOPE EQUATIONS (14/16)

with (assuming small tune shifts)

$$Q_u = Q_a - \frac{|C|}{2} \tan \alpha$$

$$Q_v = Q_b + \frac{|C|}{2} \tan \alpha$$

$$\tan(2\alpha) = \frac{|C|}{\Delta}$$

$$|C| = \frac{R^2 K}{Q_0}$$

$$\Delta = Q_b - Q_a$$

$$Q_{x0} \approx Q_{y0} \approx Q_0$$

- ◆ The solutions for the decoupled modes are $u = U e^{jQ_u \phi}$ $v = V e^{jQ_v \phi}$

where (U, V) are constants of motion, which depend on the initial conditions →

$$\Delta a = \Delta a_0 e^{jQ_u \phi} \cos \alpha - \Delta b_0 e^{jQ_v \phi} \sin \alpha$$

$$\Delta b = \Delta a_0 e^{jQ_u \phi} \sin \alpha + \Delta b_0 e^{jQ_v \phi} \cos \alpha$$

TRANSVERSE ENVELOPE EQUATIONS (15/16)

$$|\Delta a|^2 = \Delta a \Delta a^*$$

◆ Therefore,

$$|\Delta a|^2 = |\Delta a_0|^2 \cos^2 \alpha + |\Delta b_0|^2 \sin^2 \alpha - |\Delta a_0 \Delta b_0| \sin(2\alpha) \cos[(Q_v - Q_u) \phi]$$

$$|\Delta b|^2 = |\Delta a_0|^2 \sin^2 \alpha + |\Delta b_0|^2 \cos^2 \alpha + |\Delta a_0 \Delta b_0| \sin(2\alpha) \cos[(Q_v - Q_u) \phi]$$

→ $|\Delta a|^2 + |\Delta b|^2 = |\Delta a_0|^2 + |\Delta b_0|^2$

◆ Furthermore, using the fact that

$$\cos(2\alpha) = \cos\left[\arctan\left(\frac{|C|}{\Delta}\right)\right] = \left(1 + \frac{|C|^2}{\Delta^2}\right)^{-1/2}$$

→
$$\sin^2 \alpha = \frac{|C|^2 / 2}{\Delta^2 + |C|^2 + \Delta \sqrt{\Delta^2 + |C|^2}}$$

TRANSVERSE ENVELOPE EQUATIONS (16/16)

and, averaging over time (i.e. Φ), it yields (when the resonance is crossed)

$$|\Delta a|^2 = |\Delta a_0|^2 - \left(|\Delta a_0|^2 - |\Delta b_0|^2 \right) \frac{|C|^2 / 2}{\Delta^2 + |C|^2 + \Delta \sqrt{\Delta^2 + |C|^2}}$$

$$|\Delta b|^2 = |\Delta b_0|^2 + \left(|\Delta a_0|^2 - |\Delta b_0|^2 \right) \frac{|C|^2 / 2}{\Delta^2 + |C|^2 + \Delta \sqrt{\Delta^2 + |C|^2}}$$

LONGITUDINAL ENVELOPE EQUATION (1/33)

- ◆ Consider as canonical coordinates

$$\Delta\phi = \phi - \phi_s$$

$$p = \frac{h \Omega_0 \eta}{\beta^2 \gamma E_{rest}} \Delta E$$

$$\Delta\phi = \omega_{RF} \Delta t = h \Omega_0 \Delta t$$

$$\Delta E = \beta^2 E_{total} \delta$$

- ◆ The single-particle equations to be solved (far away from transition) are

$$\Delta\dot{\phi} = p$$

$$\dot{p} = F_l$$

- ◆ The total force is

$$F_l = F_l^{ext} + F_l^{SC}$$

- ◆ Without SC one has

$$F_l^{ext} = -\omega_{s0}^2 \Delta\phi$$



$$\Delta\ddot{\phi} + \omega_{s0}^2 \Delta\phi = 0$$

LONGITUDINAL ENVELOPE EQUATION (2/33)

- ◆ With SC, one can follow exactly what was done in the transverse plane, making the following replacements

$$\Delta x \rightarrow \Delta\phi$$

$$p_x \rightarrow p$$

$$K_x \rightarrow \omega_{s0}^2$$

$$\sigma_x = \sqrt{\langle \Delta x^2 \rangle} \rightarrow \tilde{\phi} = \sqrt{\langle \Delta\phi^2 \rangle}$$

$$\varepsilon_x = \sqrt{\langle \Delta x^2 \rangle \langle \Delta p_x^2 \rangle - \langle \Delta x \Delta p_x \rangle^2} \rightarrow E_0 = \sqrt{\langle \Delta\phi^2 \rangle \langle p^2 \rangle - \langle \Delta\phi p \rangle^2}$$

- ◆ Finally, the longitudinal envelope equation can be obtained

$$\ddot{\tilde{\phi}} + \omega_{s0}^2 \tilde{\phi} - \frac{E_0^2}{\tilde{\phi}^3} - \frac{\langle \Delta\phi F_l^{SC} \rangle}{\tilde{\phi}} = 0$$

LONGITUDINAL ENVELOPE EQUATION (3/33)

- Using the fact that (see "SC course")

$$F_l^{SC} = -\eta_{SC} \omega_{s0}^2 \Delta\phi, \text{ with}$$

$$\eta_{SC} = \frac{K_{sc,l}}{\Delta\hat{\phi}^3}$$

$$K_{sc,l} = \frac{3\pi N_b r_p E_{rest} g_0 h^2 \text{Sgn}(\eta)}{R \gamma^2 e \hat{V}_{RF} |\cos\phi_s|}$$

$$g_0 = 1 + 2 \ln\left(\frac{b}{a}\right)$$

$$\Delta\hat{\phi} = \pi f_0 h \tau_b$$

and the fact that

$$\frac{\langle \Delta\phi^2 \rangle}{\tilde{\phi}} = \tilde{\phi}$$

For a parabolic distribution

Half bunch length

$$\rightarrow \ddot{\tilde{\phi}} + \omega_{s0}^2 \tilde{\phi} - \frac{E_0^2}{\tilde{\phi}^3} + \frac{\omega_{s0}^2 K_{sc,l}}{\Delta\hat{\phi}^3} = 0$$

Let's now express E_0 as a function of the usual longitudinal emittance

$$\varepsilon_{l,rms} \left[\text{eVs} \right]$$

LONGITUDINAL ENVELOPE EQUATION (4/33)

$$\Delta\phi = \omega_{RF} t = h \Omega_0 t$$

$$p = \frac{h \Omega_0 \eta}{\beta^2 \gamma E_{rest}} \Delta E$$



$$p \Delta\phi = \frac{h^2 \Omega_0^2 \eta}{\beta^2 \gamma E_{rest}} \Delta E t$$



$$E_0 = \frac{h^2 \Omega_0^2 |\eta|}{\beta^2 \gamma E_{rest}} \times \frac{\varepsilon_{l,rms} [\text{eVs}]}{\pi}$$

- ◆ Now, let's convert the envelope equation to one for the half bunch length $\Delta\hat{\phi}$. For a parabolic distribution

$$\Delta\hat{\phi} = \sqrt{5} \tilde{\phi}$$

LONGITUDINAL ENVELOPE EQUATION (5/33)

$$\rightarrow \Delta \ddot{\hat{\phi}} + \omega_{s0}^2 \Delta \hat{\phi} + \frac{\omega_{s0}^2 K_{sc,l}}{\Delta \hat{\phi}^2} - \frac{25 E_0^2}{\Delta \hat{\phi}^3} = 0$$

Envelope equation for the half bunch length far from transition

- ◆ Let's now derive the evolution of the phase space ellipse near transition (before deriving the envelope equation near transition)

Synchrotron oscillations equation

$$\frac{d \Delta \phi}{d t} = \frac{h \eta \Omega_0}{\beta^2 E_{total}} \Delta E$$

$$\frac{d \Delta E}{d t} = \frac{e \hat{V}_{RF} \Omega_0}{2 \pi} \left[\sin(\phi_s + \Delta \phi) - \sin \phi_s \right] \approx \frac{e \hat{V}_{RF} \Omega_0}{2 \pi} \cos \phi_s \Delta \phi$$

LONGITUDINAL ENVELOPE EQUATION (6/33)

$$\rightarrow \frac{d}{dt} \left(\frac{\beta^2 E_{total}}{h \eta \Omega_0} \frac{d \Delta \phi}{dt} \right) - \frac{e \hat{V}_{RF} \Omega_0}{2 \pi} \cos \phi_s \Delta \phi = 0$$

with β , E_{total} , η , Ω_0 which depend on time t

Approximation: We neglect the slow time variations of all the parameters except

$$\frac{\eta}{E_{total}}$$

$$\rightarrow \frac{d}{dt} \left(\frac{E_{total}}{\eta} \frac{d \Delta \phi}{dt} \right) - \frac{h e \hat{V}_{RF} \Omega_0^2 \cos \phi_s}{2 \pi \beta^2} \Delta \phi = 0$$

Assumed to be time independent

LONGITUDINAL ENVELOPE EQUATION (7/33)

Furthermore, $\gamma = \gamma_t + \dot{\gamma} t$, with $t < 0$ below transition and $t > 0$ above transition

$$\rightarrow \eta = \frac{1}{\gamma_t^2} - \frac{1}{\gamma^2} \approx \frac{2 \dot{\gamma} t}{\gamma_t^3} \quad \text{and} \quad E_{total} = \gamma E_{rest} \approx \gamma_t E_{rest}$$

$$\rightarrow \frac{\eta}{E_{total}} \approx \frac{2 \dot{\gamma} t}{\gamma_t^4 E_{rest}}$$

$$\rightarrow \frac{d}{dt} \left(\frac{1}{\omega_{s0}^2} \frac{d \Delta \phi}{dt} \right) + \Delta \phi = 0 \quad \text{with} \quad \omega_{s0} = \Omega_0 \left(-\frac{e \hat{V}_{RF} h \eta \cos \phi_s}{2 \pi \beta^2 E_{total}} \right)^{1/2}$$

But here, this should be considered as a definition only, as the beam particle do not make synchrotron oscillations and therefore it loses its meaning of oscillation frequency

LONGITUDINAL ENVELOPE EQUATION (8/33)

One can write $\omega_{s0}^2 = \frac{|t|}{T_c^3}$, with $T_c = \left(\frac{\beta^2 E_{rest} \gamma_t^4}{4 \pi f_0^2 \dot{\gamma} h e \hat{V}_{RF} |\cos \phi_s|} \right)^{1/3}$

It is called the nonadiabatic time

Physical meaning of the nonadiabatic time: When the time is close enough to transition, the particle will not be able to catch up with the rapid changing of the bucket shape

→ One has to solve

$$\frac{d}{dt} \left(\frac{T_c^3}{|t|} \frac{d \Delta \phi}{dt} \right) + \Delta \phi = 0$$

LONGITUDINAL ENVELOPE EQUATION (9/33)

Defining a new time variable, and considering only $t > 0$ for the moment

$$y = \int_0^x \sqrt{u} \, du = \frac{2}{3} x^{3/2}$$

$$x = \frac{t}{T_c}$$

→ One has to solve

$$\frac{d}{dx} \left(\frac{1}{x} \frac{d \Delta\phi}{dx} \right) + \Delta\phi = 0$$

Let's call $\Delta\phi = \varphi y^{2/3}$

→

$$\frac{d^2 \varphi}{dy^2} + \frac{1}{y} \frac{d\varphi}{dy} + \left[1 - \frac{\left(\frac{2}{3}\right)^2}{y^2} \right] \varphi = 0$$

LONGITUDINAL ENVELOPE EQUATION (10/33)

The solution of this equation can be written

$$\varphi = C_1 J_{2/3}(y) + C_2 N_{2/3}(y) = C_3 \left[J_{2/3}(y) \cos \chi + N_{2/3}(y) \sin \chi \right]$$

Constants to be determined from the initial conditions

with $J_{2/3}$ the Bessel function of the 1st kind (or simply the Bessel function), and $N_{2/3}$ the Bessel function of the 2nd kind (also called Weber or Neumann function)

→ $\Delta\phi = b x \left[J_{2/3}(y) \cos \chi + N_{2/3}(y) \sin \chi \right]$

Constants to be determined from the initial conditions

LONGITUDINAL ENVELOPE EQUATION (11/33)

$$\Delta E = \beta^2 E_{total} \delta$$

$$\delta = \frac{\Delta p}{p_0}$$

and

$$\Delta E = \frac{\beta^2 E_{total}}{h \Omega_0 \eta} \frac{d \Delta \phi}{d t}$$

→

$$\delta = \frac{1}{h \Omega_0 \eta} \frac{d \Delta \phi}{d t} = \frac{\gamma_t^3}{2 \dot{\gamma} t h \Omega_0} \frac{d \Delta \phi}{d t}$$

$$\rightarrow \delta = \frac{\gamma_t^3}{2 \dot{\gamma} t h \Omega_0} \left\{ \frac{\Delta \phi}{x T_c} + \frac{b x^{3/2}}{T_c} \left[\left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right) \cos \chi + \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right) \sin \chi \right] \right\}$$

using the fact that

$$J'_n(y) = \frac{n}{y} J_n(y) - J_{n+1}(y)$$

$$N'_n(y) = \frac{n}{y} N_n(y) - N_{n+1}(y)$$

LONGITUDINAL ENVELOPE EQUATION (12/33)

Now the idea is, with the 2 equations

$$\Delta\phi = b x \left[J_{2/3}(y) \cos \chi + N_{2/3}(y) \sin \chi \right]$$

$$\delta = \frac{\gamma_t^3}{2 \dot{\gamma} t h \Omega_0} \left\{ \frac{\Delta\phi}{x T_c} + \frac{b x^{3/2}}{T_c} \left[\left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right) \cos \chi + \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right) \sin \chi \right] \right\}$$

to solve for $\cos \chi$ and $\sin \chi$, and then write the equation

$$\cos^2 \chi + \sin^2 \chi = 1 \quad \text{to derive an equation linking } \Delta\phi \text{ and } \delta$$

$$\rightarrow \alpha_{\phi\phi} \Delta\phi^2 + 2 \alpha_{\phi\delta} \Delta\phi \delta + \alpha_{\delta\delta} \delta^2 = 1$$

LONGITUDINAL ENVELOPE EQUATION (13/33)

with

$$\alpha_{\phi\phi} = \frac{1}{\det^2 b^2 x^2} \left\{ \begin{aligned} & \frac{J_{2/3}^2}{x^3} + \left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right)^2 + \frac{2 J_{2/3}}{x^{3/2}} \left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right) \\ & + \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right)^2 + \frac{N_{2/3}^2}{x^3} + \frac{2 N_{2/3}}{x^{3/2}} \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right) \end{aligned} \right\}$$

$$\alpha_{\delta\delta} = \frac{1}{\det^2 b^2 x^3} \left(\frac{2 \dot{\gamma} t h \Omega_0 T_c}{\gamma_t^3} \right)^2 (J_{2/3}^2 + N_{2/3}^2)$$

$$\alpha_{\phi\delta} = \frac{1}{\det^2} \left\{ \begin{aligned} & - \frac{2 J_{2/3}^2 T_c h \Omega_0 \dot{\gamma} t}{b^2 x^4 \gamma_t^3} - \frac{J_{2/3} T_c}{b^2 x^{5/2} \gamma_t^3} \left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right) 2 \dot{\gamma} t h \Omega_0 \\ & - \frac{2 N_{2/3}^2 T_c h \Omega_0 \dot{\gamma} t}{b^2 x^4 \gamma_t^3} - \frac{N_{2/3} T_c}{b^2 x^{5/2} \gamma_t^3} \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right) 2 \dot{\gamma} t h \Omega_0 \end{aligned} \right\}$$

$$\det = J_{2/3} \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right) - N_{2/3} \left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right)$$

LONGITUDINAL ENVELOPE EQUATION (14/33)

Using the fact that

$$J_{\alpha}(y) N'_{\alpha}(y) - J'_{\alpha}(y) N_{\alpha}(y) = \frac{2}{\pi y}$$

→

$$\det = J_{2/3} \left(\frac{2 N_{2/3}}{3 y} - N_{5/3} \right) - N_{2/3} \left(\frac{2 J_{2/3}}{3 y} - J_{5/3} \right) = J_{2/3} N'_{2/3} - N_{2/3} J'_{2/3} = \frac{2}{\pi y}$$

→

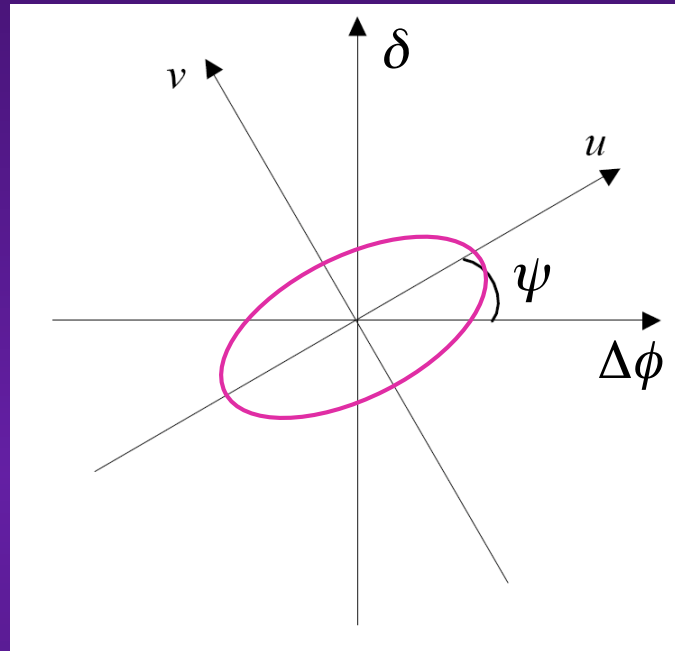
$$\alpha_{\phi\phi} = \frac{\pi^2}{9 b^2 x^2} \left\{ \left(2 J_{2/3} - \frac{3 y}{2} J_{5/3} \right)^2 + \left(2 N_{2/3} - \frac{3 y}{2} N_{5/3} \right)^2 \right\}$$

$$\alpha_{\delta\delta} = \frac{\pi^2 x^2}{9 b^2} \left(\frac{2 \dot{\gamma} h \Omega_0 T_c^2}{\gamma_t^3} \right)^2 (J_{2/3}^2 + N_{2/3}^2)$$

$$\alpha_{\phi\delta} = \frac{\pi^2}{9 b^2} \left(\frac{2 \dot{\gamma} h \Omega_0 T_c^2}{\gamma_t^3} \right) \left[N_{2/3} \left(\frac{3 y}{2} N_{5/3} - 2 N_{2/3} \right) - J_{2/3} \left(2 J_{2/3} - \frac{3 y}{2} J_{5/3} \right) \right]$$

LONGITUDINAL ENVELOPE EQUATION (15/33)

Let's now compute the emittance of the tilted ellipse



Method: Let's find (u, v) where the ellipse is upright

$$\begin{pmatrix} \Delta\phi \\ \delta \end{pmatrix} = \begin{bmatrix} \cos\psi & -\sin\psi \\ \sin\psi & \cos\psi \end{bmatrix} \begin{pmatrix} u \\ v \end{pmatrix}$$

LONGITUDINAL ENVELOPE EQUATION (16/33)

=> The ellipse is upright if

$$\psi = \frac{1}{2} \arctan \left(\frac{2 \alpha_{\phi\delta}}{\alpha_{\phi\phi} - \alpha_{\delta\delta}} \right)$$

It is the tilt angle of the ellipse

Using the fact that

$$\cos(\arctan x) = \frac{1}{\sqrt{1+x^2}}$$

$$\sin(\arctan x) = \frac{x}{\sqrt{1+x^2}}$$

the equation of the ellipse can be written

$$\frac{1}{2} \left[\alpha_{\phi\phi} + \alpha_{\delta\delta} + \sqrt{(\alpha_{\phi\phi} - \alpha_{\delta\delta})^2 + 4 \alpha_{\phi\delta}^2} \right] u^2 + \frac{1}{2} \left[\alpha_{\phi\phi} + \alpha_{\delta\delta} - \sqrt{(\alpha_{\phi\phi} - \alpha_{\delta\delta})^2 + 4 \alpha_{\phi\delta}^2} \right] v^2 = 1$$

LONGITUDINAL ENVELOPE EQUATION (17/33)

The area of the ellipse is thus

$$A = \pi \sqrt{\frac{2}{\alpha_{\phi\phi} + \alpha_{\delta\delta} + \sqrt{(\alpha_{\phi\phi} - \alpha_{\delta\delta})^2 + 4\alpha_{\phi\delta}^2}}} \sqrt{\frac{2}{\alpha_{\phi\phi} + \alpha_{\delta\delta} - \sqrt{(\alpha_{\phi\phi} - \alpha_{\delta\delta})^2 + 4\alpha_{\phi\delta}^2}}}$$



$$A = \frac{\pi}{\sqrt{\alpha_{\phi\phi} \alpha_{\delta\delta} - \alpha_{\phi\delta}^2}}$$

and

$$A = \varepsilon_l [\text{eVs}] \frac{h \Omega_0}{\beta^2 E_{total}}$$

Using the fact that

$$J_{2/3} \left(\frac{3y N_{5/3}}{2} - 2 N_{2/3} \right) + N_{2/3} \left(2 J_{2/3} - \frac{3y J_{5/3}}{2} \right) = -\frac{3}{\pi}$$

LONGITUDINAL ENVELOPE EQUATION (18/33)

=> The remaining unknown b can be found and is given by

$$b = \sqrt{\frac{2 \varepsilon_l h^2 \Omega_0^2 \dot{\gamma} T_c^2}{3 m_0 c^2 \beta^2 \gamma_t^4}}$$

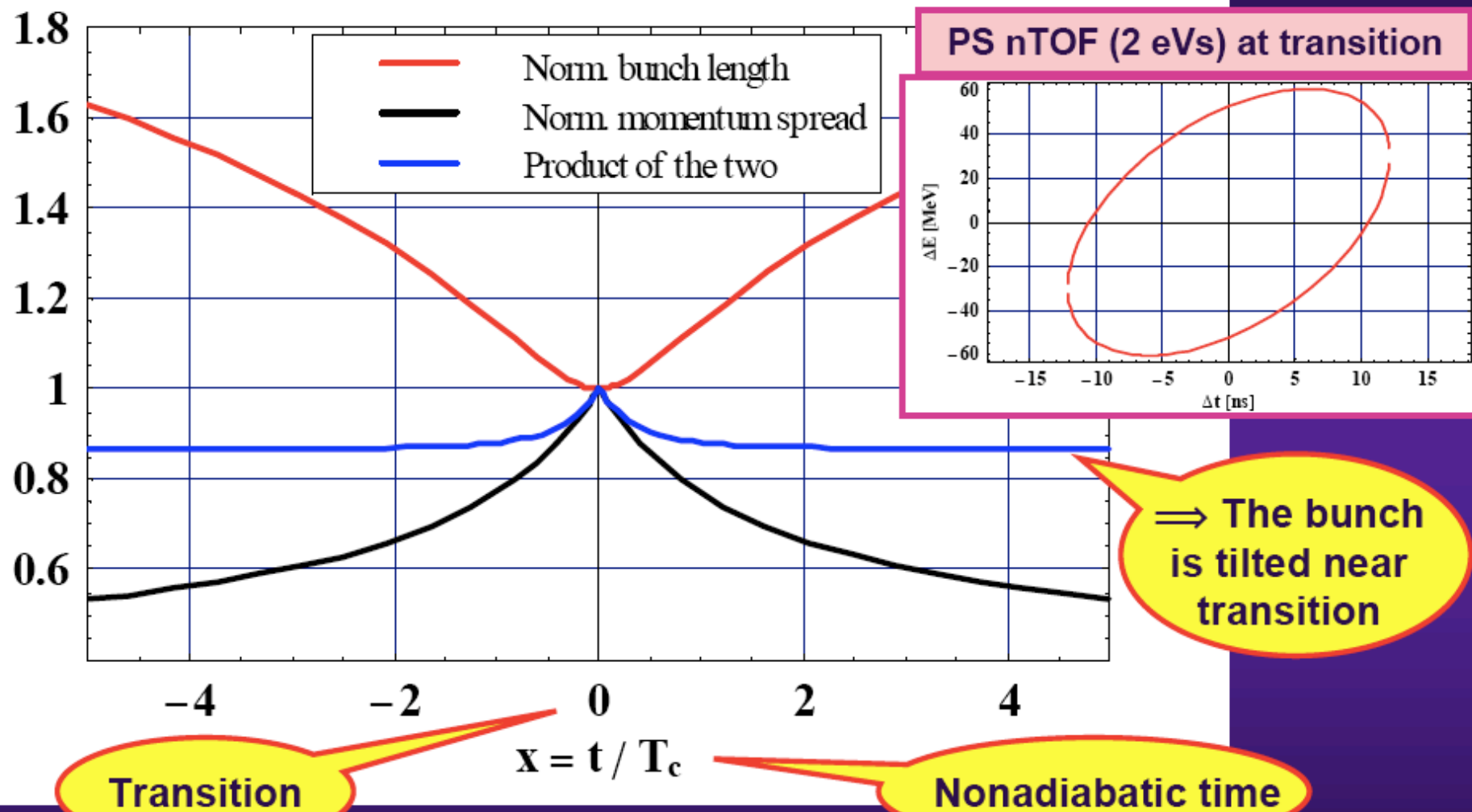
One now has all the parameters of the ellipse which can be plotted at any time t => The evolution of the bunch length, the energy spread and the phase space ellipse can be studied near transition

$$\Delta\phi_{\max} = \frac{\sqrt{\alpha_{\delta\delta}}}{\sqrt{\alpha_{\phi\phi} \alpha_{\delta\delta} - \alpha_{\phi\delta}^2}}$$

$$\delta_{\max} = \frac{\sqrt{\alpha_{\phi\phi}}}{\sqrt{\alpha_{\phi\phi} \alpha_{\delta\delta} - \alpha_{\phi\delta}^2}}$$

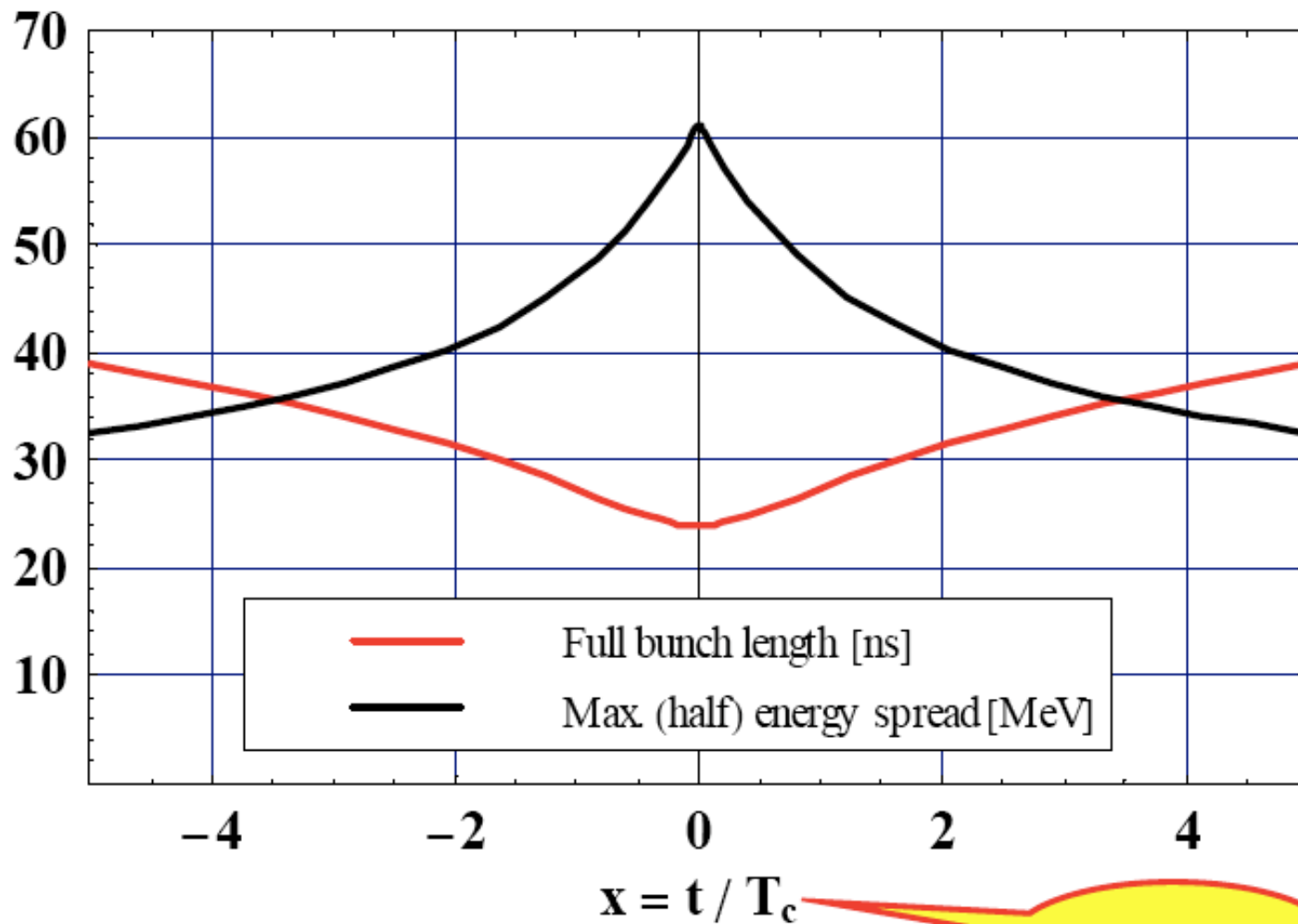
Properties in an ellipse
(see "Introduction")

LONGITUDINAL ENVELOPE EQUATION (19/33)



LONGITUDINAL ENVELOPE EQUATION (20/33)

Case of the CERN PS nTOF bunch without SC



$$x = t / T_c$$

$$T_c \approx 1.9 \text{ ms}$$

$$\varepsilon_L = 2 \text{ eVs}$$

LONGITUDINAL ENVELOPE EQUATION (21/33)

- ◆ Let's now concentrate on the derivation of the envelope equation NEAR TRANSITION. Far from transition, the envelope equation was found to be

$$\Delta\ddot{\hat{\phi}} + \omega_{s0}^2 \Delta\hat{\phi} + \frac{\omega_{s0}^2 K_{sc,l}}{\Delta\hat{\phi}^2} - \frac{25 E_0^2}{\Delta\hat{\phi}^3} = 0$$

which can also be written

$$\frac{1}{\omega_{s0}^2} \frac{d^2 \tau_b}{dt^2} + \tau_b + \frac{K_{sc,l1}}{\tau_b^2} - \frac{S_1}{\tau_b^3} = 0$$

with

$$K_{sc,l1} = \frac{K_{sc,l}}{\pi^3 h^3 f_0^3} = \frac{3 N_b r_p E_{rest} g_0 \text{Sgn}(\eta)}{\pi^2 h f_0^3 R \gamma_t^2 e \hat{V}_{RF} |\cos \phi_s|}$$

$$S_1 = \frac{16 \eta^2 \varepsilon_l^2}{\pi^2 \beta^4 \gamma^2 E_{rest}^2 \omega_{s0}^2}$$

$$\varepsilon_l = 5 \varepsilon_{l,rms}$$

LONGITUDINAL ENVELOPE EQUATION (22/33)

Close to transition

$$x = \frac{t}{T_c}$$

$$\omega_{s0}^2 = \frac{|t|}{T_c^3}$$



$$\omega_{s0}^2 = \frac{|x|}{T_c^2}$$



$$\frac{1}{|x|} \frac{d^2 \tau_b}{d x^2} + \tau_b + \frac{K_{sc,l1}}{\tau_b^2} - \frac{S_1}{\tau_b^3} = 0$$

Knowing that, close to transition, one has to make the substitution (as seen in the previous slides)

$$\frac{1}{|x|} \frac{d^2 \tau_b}{d x^2}$$



$$\frac{d}{d x} \left(\frac{1}{|x|} \frac{d \tau_b}{d x} \right)$$

LONGITUDINAL ENVELOPE EQUATION (23/33)

→ One has to solve

$$\frac{d}{dx} \left(\frac{1}{|x|} \frac{d\tau_b}{dx} \right) + \tau_b + \frac{K_{sc,l1}}{\tau_b^2} - \frac{S_1}{\tau_b^3} = 0$$

which can also be written

$$\frac{d}{dx} \left(\frac{1}{|x|} \frac{d\tau_{bns}}{dx} \right) + \tau_{bns} + \frac{10^{27} K_{sc,l1}}{\tau_{bns}^2} - \frac{10^{36} |x| S_2}{\tau_{bns}^3} = 0$$

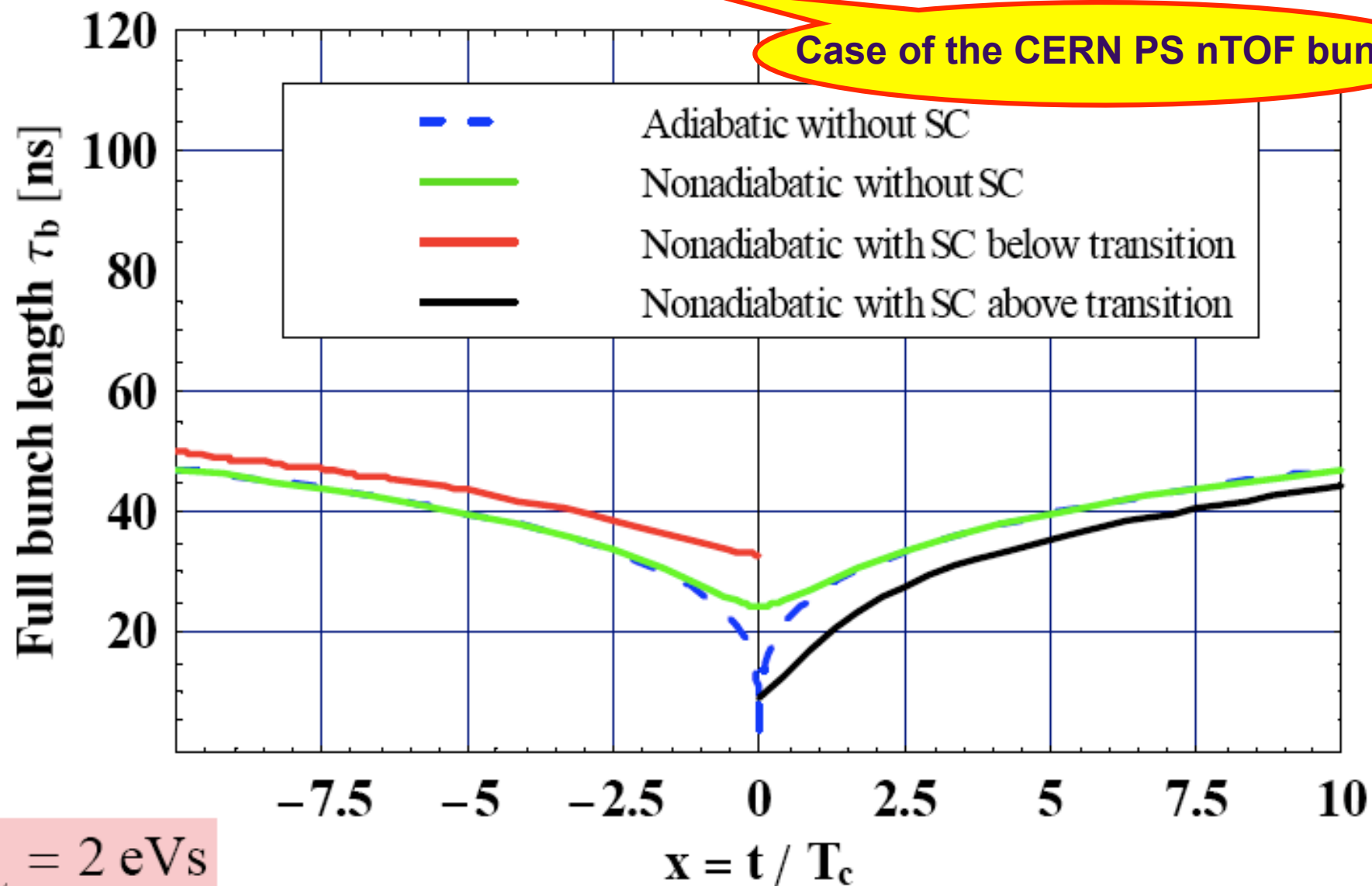
with

$$S_2 = \frac{64 \varepsilon_l^2 \dot{\gamma}^2 T_c^4}{\pi^2 \beta^4 \gamma_t^8 E_{rest}^2}$$

Full (4σ) bunch length in ns

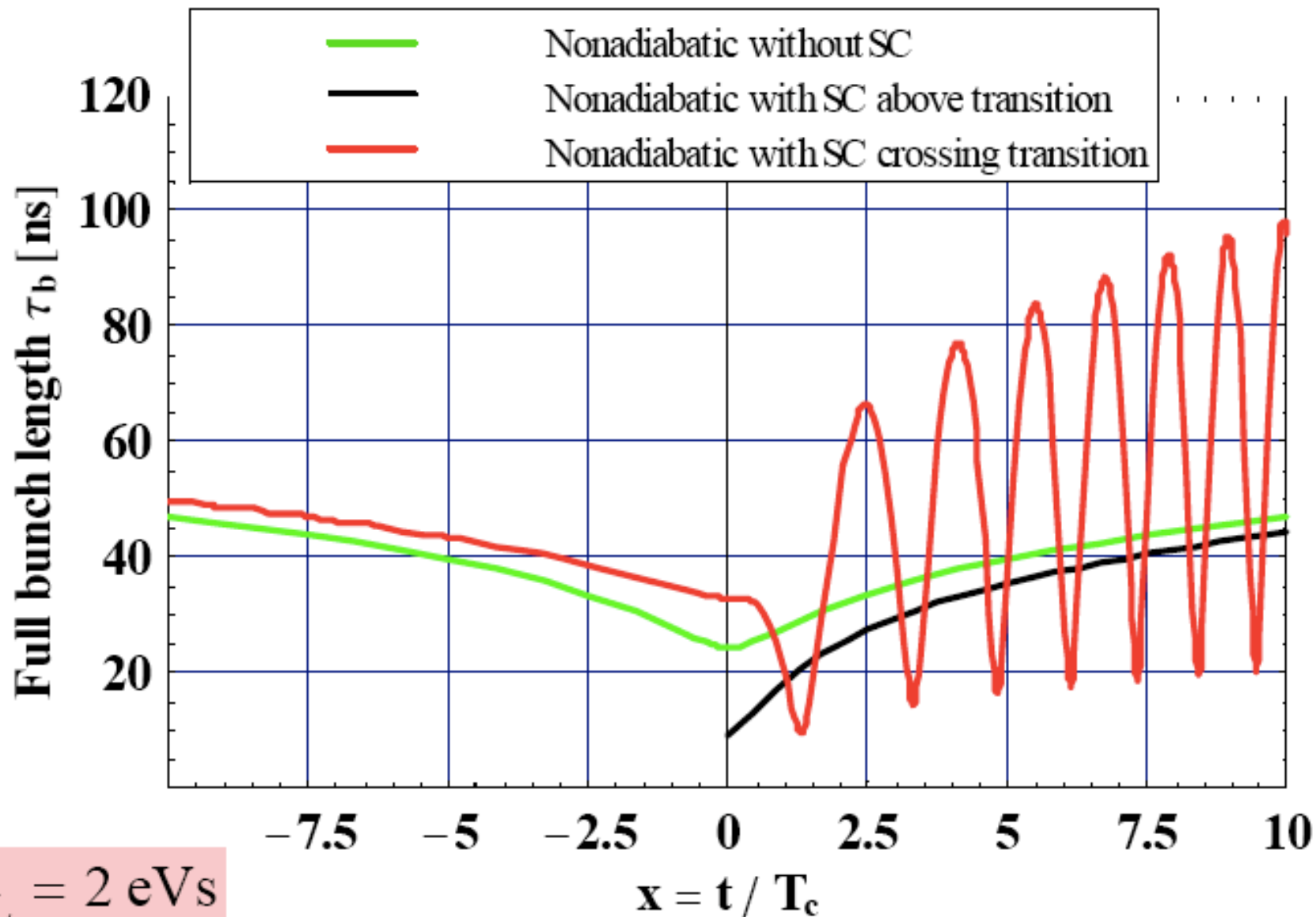
LONGITUDINAL ENVELOPE EQUATION (24/33)

STATIC (MATCHED) CASE



LONGITUDINAL ENVELOPE EQUATION (25/33)

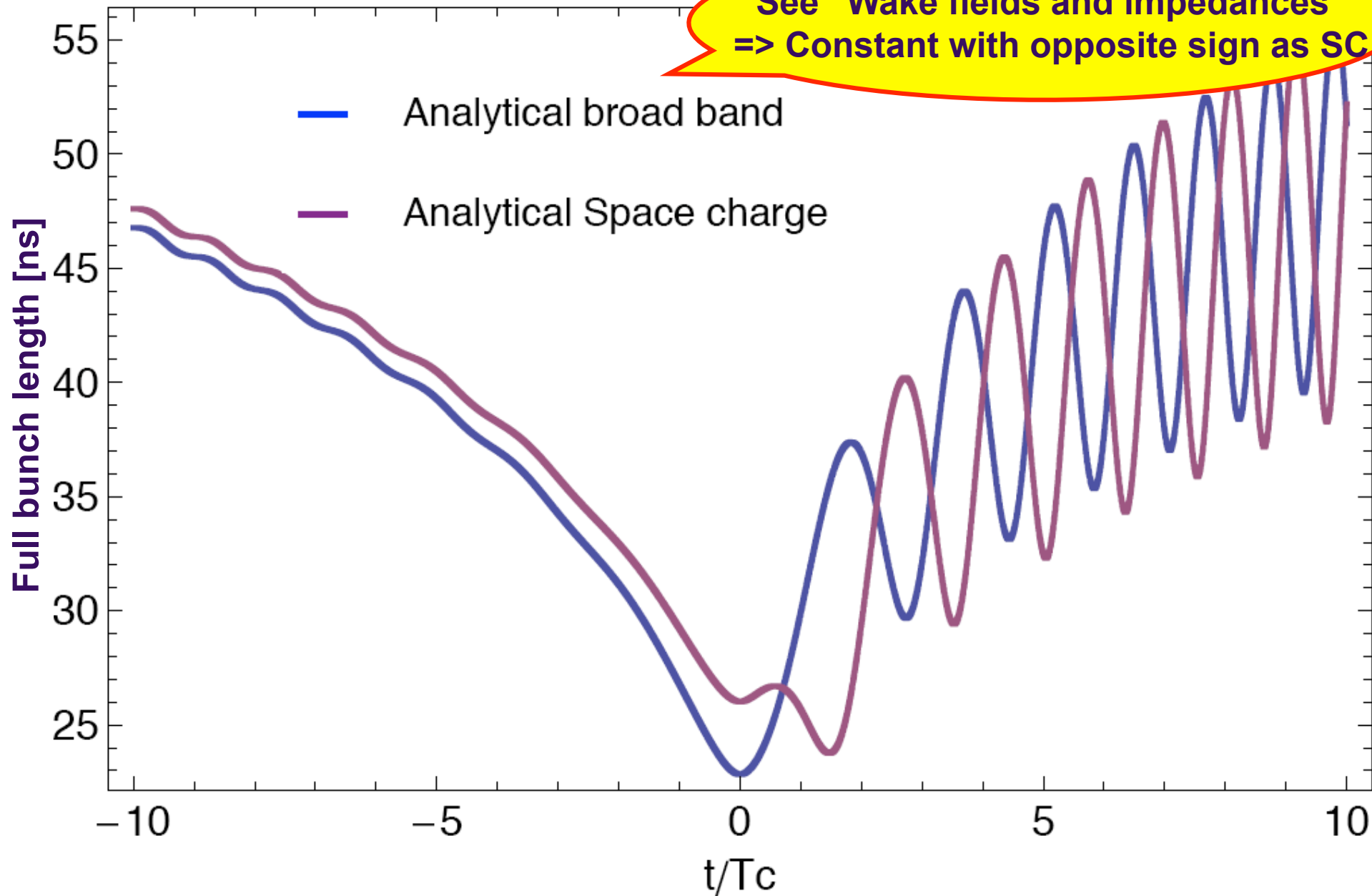
DYNAMIC (“REAL”) CASE WHEN TRANSITION IS CROSSED



$\epsilon_L = 2 \text{ eVs}$

LONGITUDINAL ENVELOPE EQUATION (26/33)

See "Wake fields and impedances"
=> Constant with opposite sign as SC



LONGITUDINAL ENVELOPE EQUATION (27/33)

- ◆ **Bunch rotation with SC (and or constant inductive impedance)**

=> The envelope equation can also be used to estimate, for a given compression factor, the needed RF voltage, the compression time, the evolution of the bunch length and the evolution of the momentum spread

- ◆ **The envelope equation can also be (sometimes) written**

$$\frac{d^2 r_z}{dz^2} + K_{RF} r_z - \frac{K_{sc,l2}}{r_z^2} - \frac{\epsilon_{l2}^2}{r_z^3} = 0$$

Half bunch length (in meters)

$$K_{RF} = \frac{e \hat{V}_{RF} h |\eta \cos \phi_s|}{2\pi R^2 \gamma \beta^2 m_0 c^2}$$

$$K_{sc,l2} = \frac{3 \hat{g} r_p N_b |\eta|}{2\gamma^3 \beta^2}$$

Depends on the source (was 1 before)

$$\hat{g} = \frac{1}{2} + 2 \ln \left(\frac{r_{pipe}}{r_{beam}} \right)$$

$$\epsilon_{l2} = |\eta| r_{z0} \frac{\Delta p}{p_0} = cte$$

LONGITUDINAL ENVELOPE EQUATION (28/33)

- ◆ The bunch is matched (at constant energy) when

$$r_z = r_{z0} \Rightarrow$$

$$\frac{d^2 r_z}{dz^2} = \frac{dr_z}{dz} = 0$$

- ◆ Before, we used $\Delta\hat{\phi}$ and we had

$$\Delta\hat{\phi} = \pi h f_0 \tau_b$$

Full bunch length [in s]

- ◆ Here, we use r_z and we have

$$r_z = \beta c \frac{\tau_b}{2}$$

- ◆ It can be checked that this equation is the same as the one we used before (with the small difference on the g-factor), remembering that

Used before

$$\varepsilon_l = \frac{\pi}{2} \beta^2 \gamma E_{rest} \tau_b \frac{\Delta p}{p_0}$$

LONGITUDINAL ENVELOPE EQUATION (29/33)

- ◆ Example of bunch rotation estimated in the past in a 2 GeV proton-accumulator-compressor for a neutrino factory

$$\hat{V}_{RF} = 7 \text{ MV}$$

$$h = 24$$

$$N_b = 10^{13} \text{ p/b}$$

$$\tau_b = 50 \text{ ns}$$

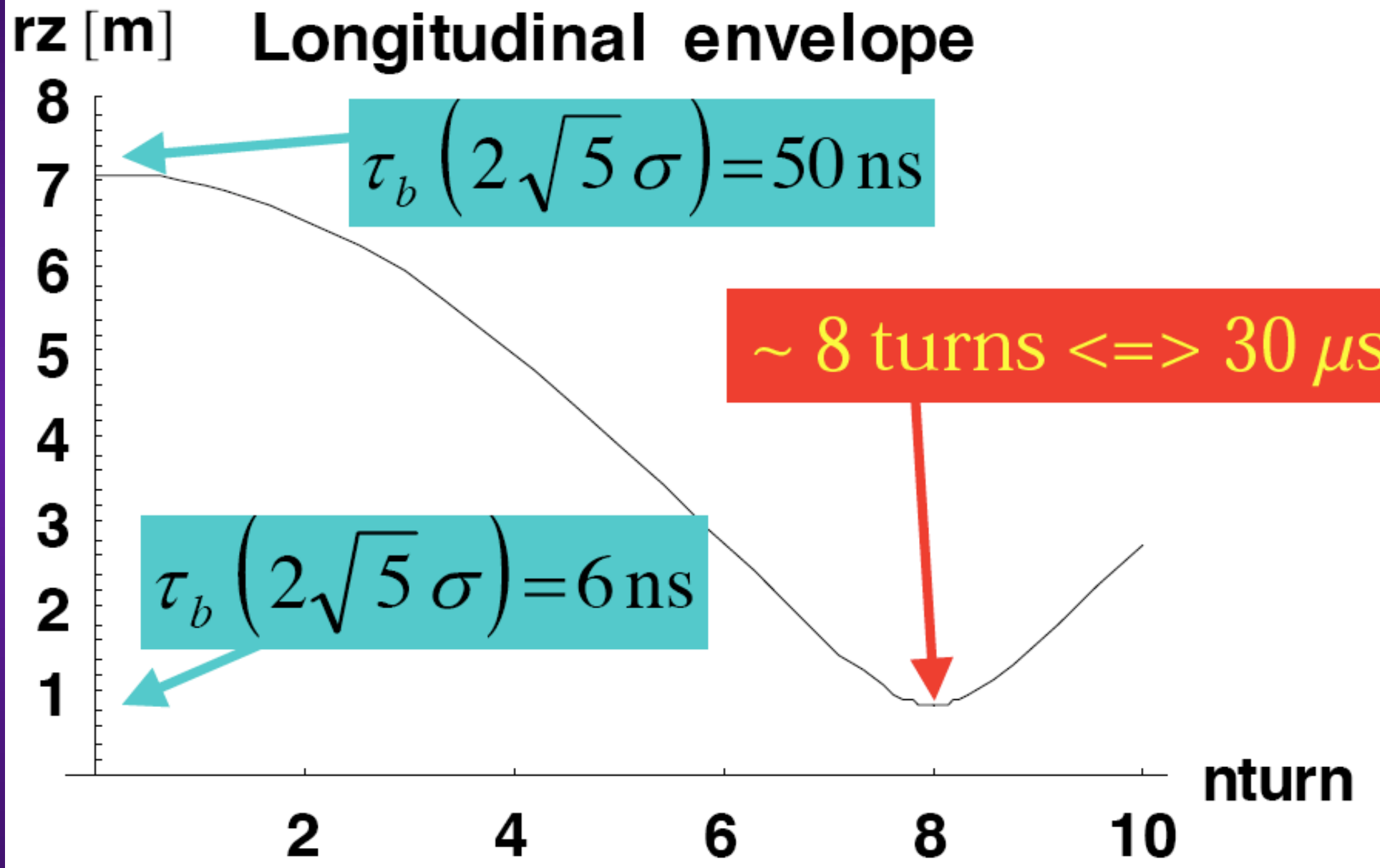
$$\left(\Delta p / p_0 \right)_{\max} = 2 \left(\sigma_p / p_0 \right) = 1.5 \times 10^{-3}$$

$$R = 150 \text{ m}$$

$$\eta = -0.1$$

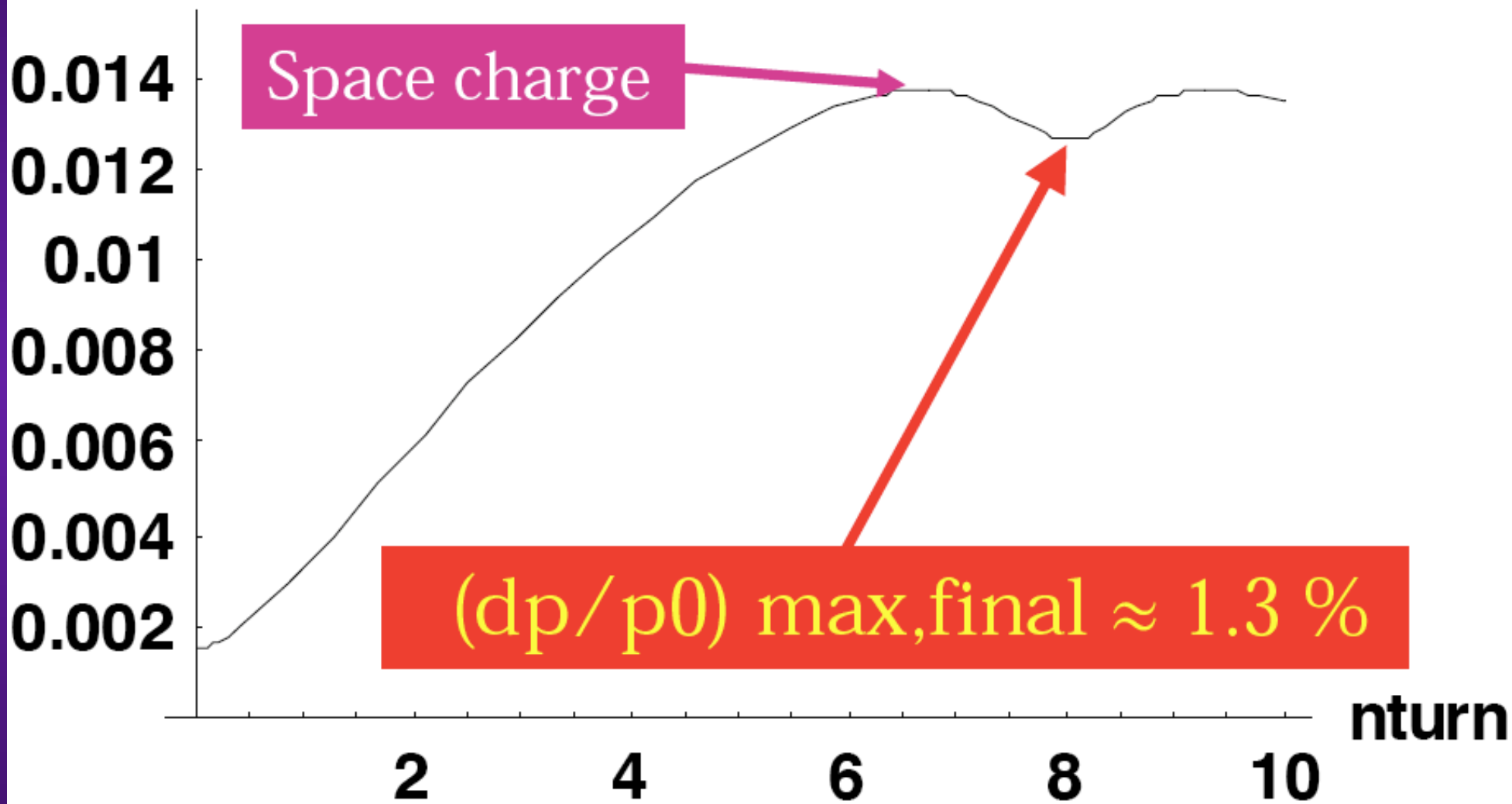
$$\hat{g} \approx 4$$

LONGITUDINAL ENVELOPE EQUATION (30/33)

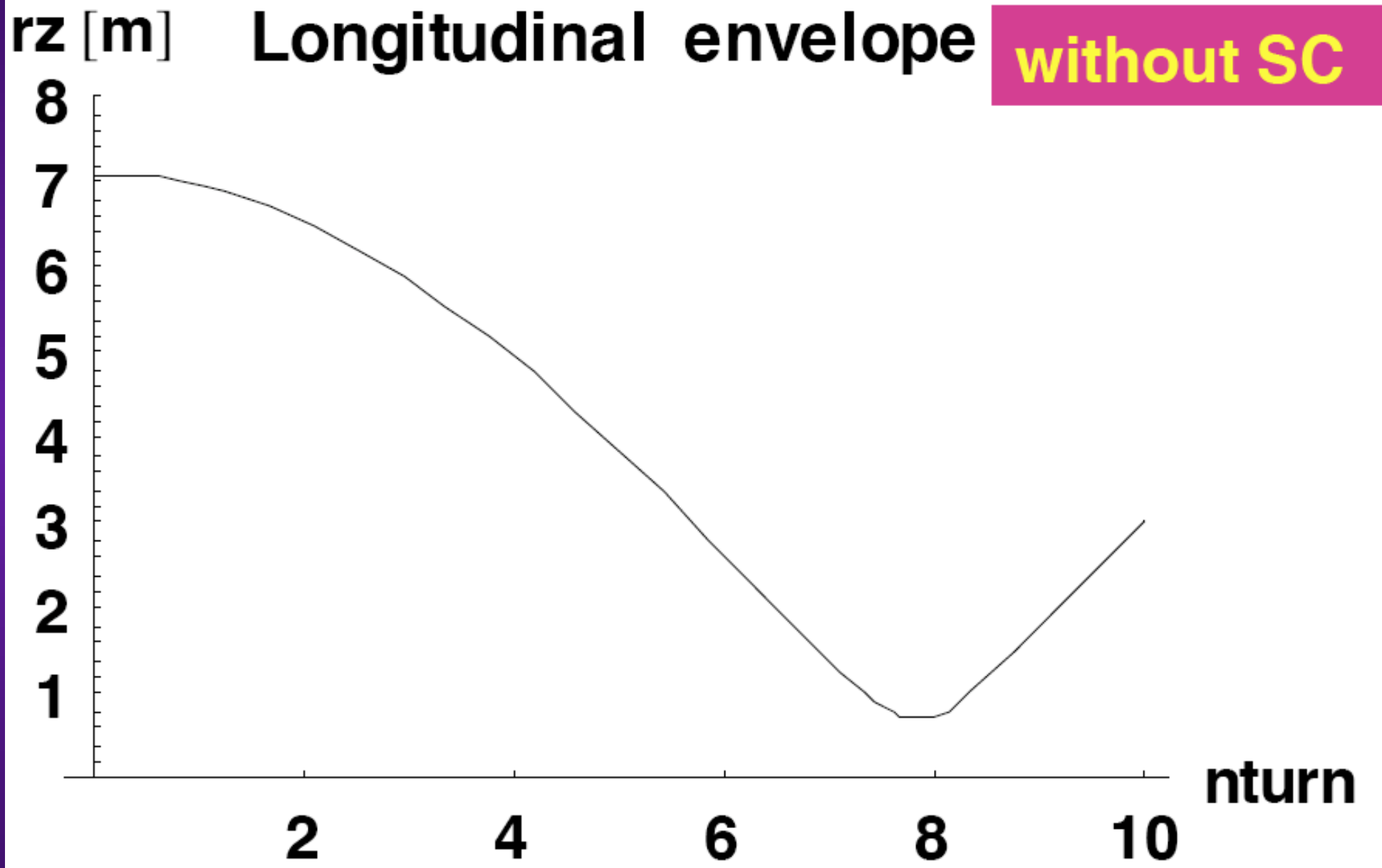


LONGITUDINAL ENVELOPE EQUATION (31/33)

(dp/p_0) max Momentum spread



LONGITUDINAL ENVELOPE EQUATION (32/33)



LONGITUDINAL ENVELOPE EQUATION (33/33)

(dp/p0) max Momentum spread

without SC

